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(54) **FUEL INJECTOR WITH A DIFFUSING MAIN GAS PASSAGE**

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See application file for complete search history.

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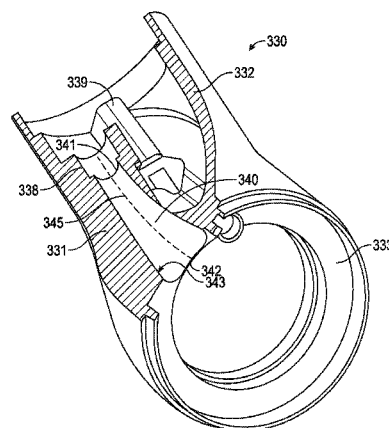
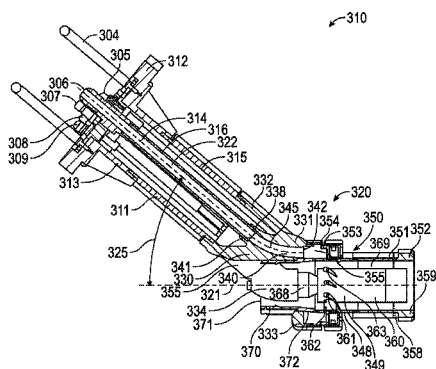
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(57) **ABSTRACT**

A fuel injector for a combustor of a gas turbine engine is disclosed. The fuel injector includes a gas gallery and a gas passage. The gas gallery is an annular passage configured to circumferentially distribute gas fuel. The gas passage includes an inlet and an outlet. The inlet is distal to the gas gallery and includes an inlet area with a circular shape. The outlet adjoins the gas gallery and includes an outlet area including an annular sector shape. The gas passage is configured to diffuse the gas fuel and discharge the gas fuel from the outlet and into the gas gallery.

20 Claims, 4 Drawing Sheets



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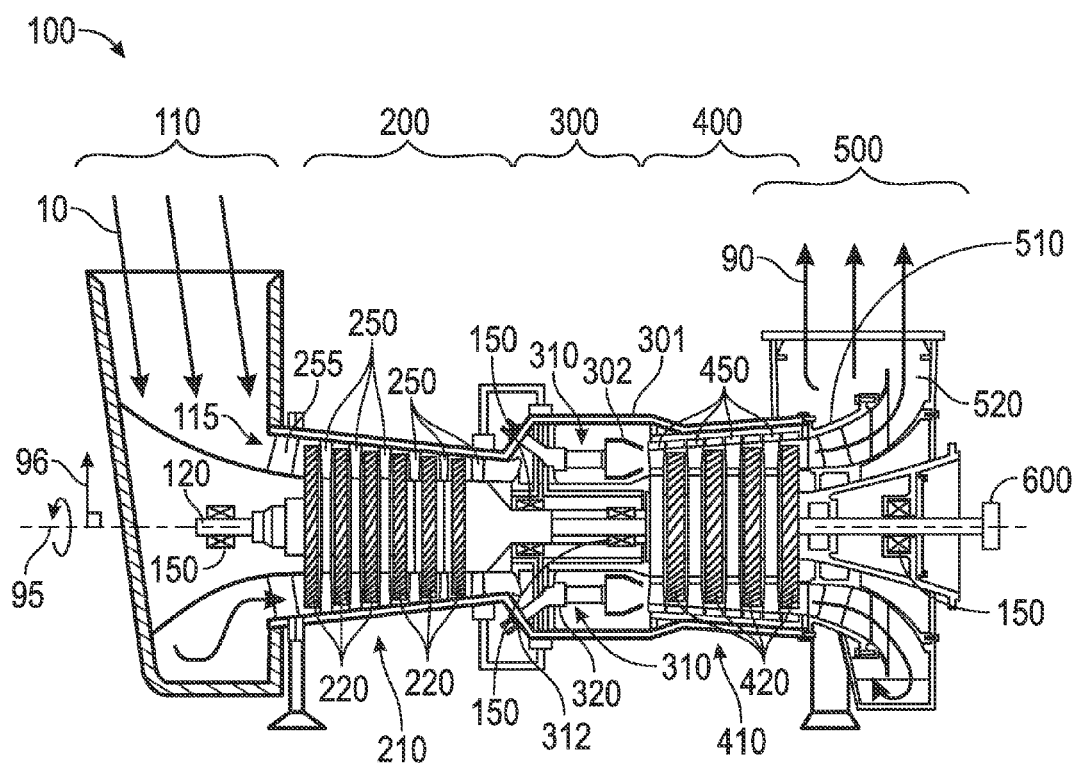


FIG. 1

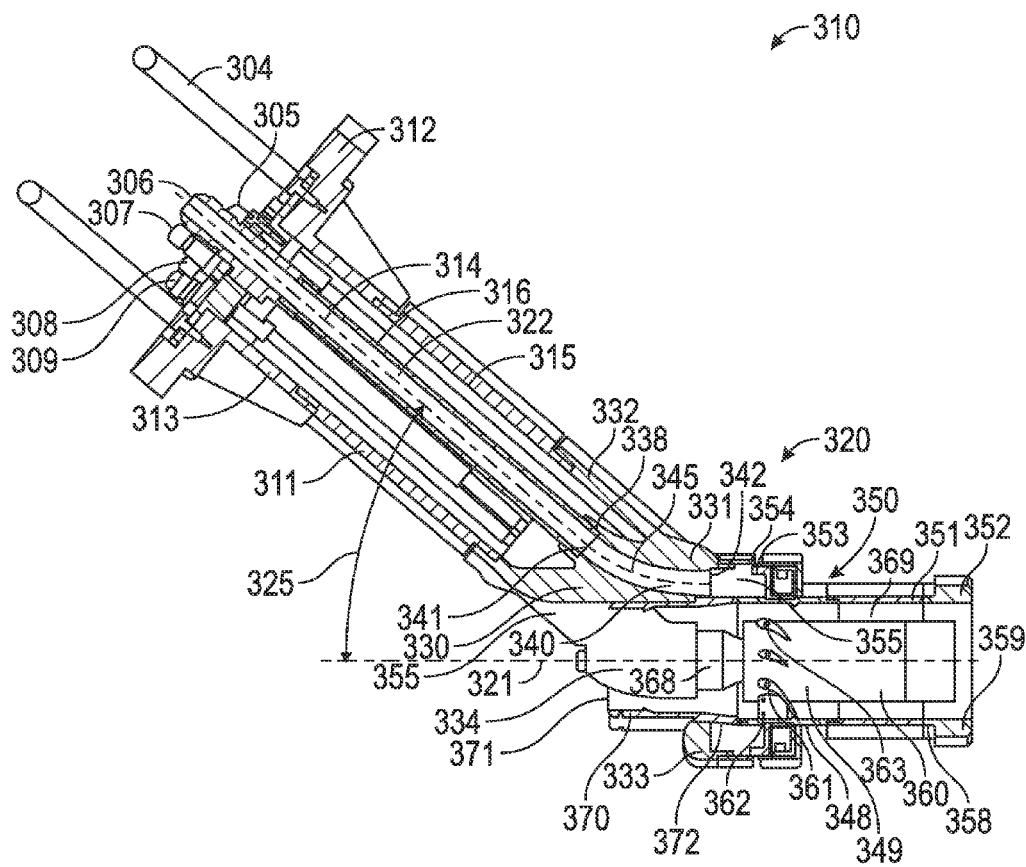


FIG. 2

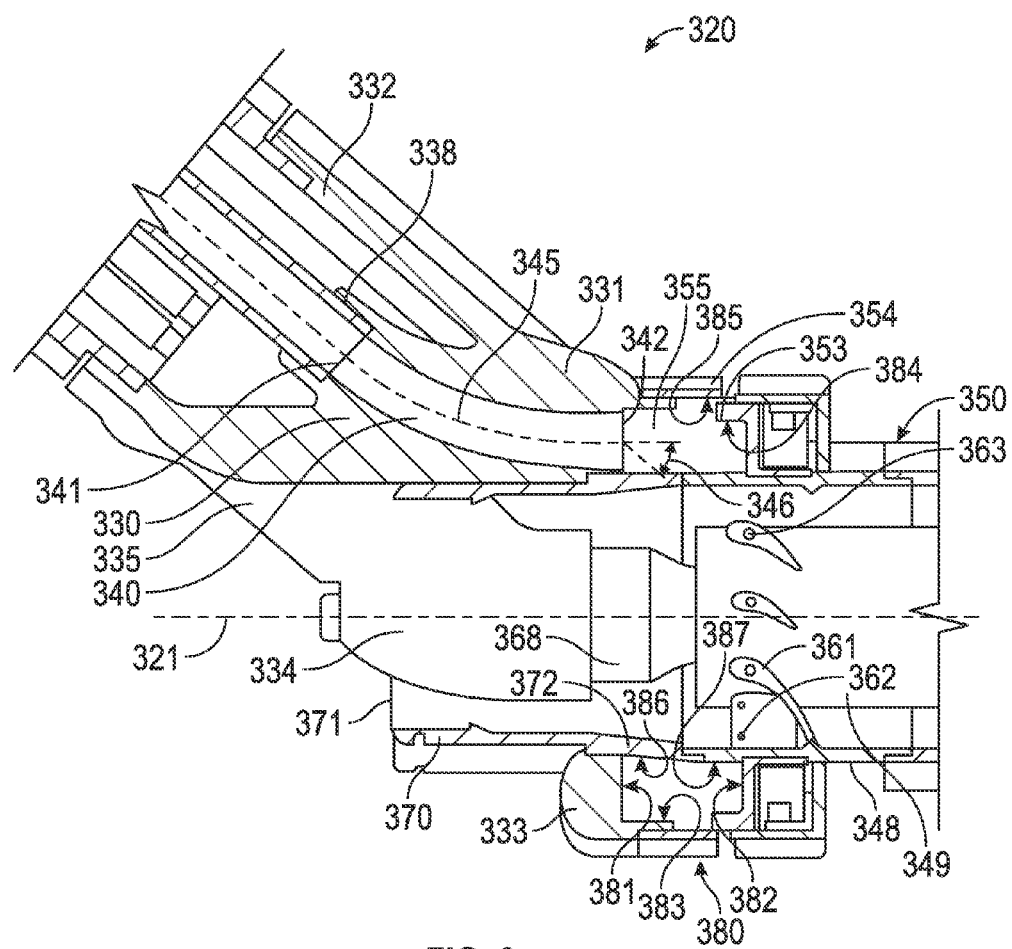


FIG. 3

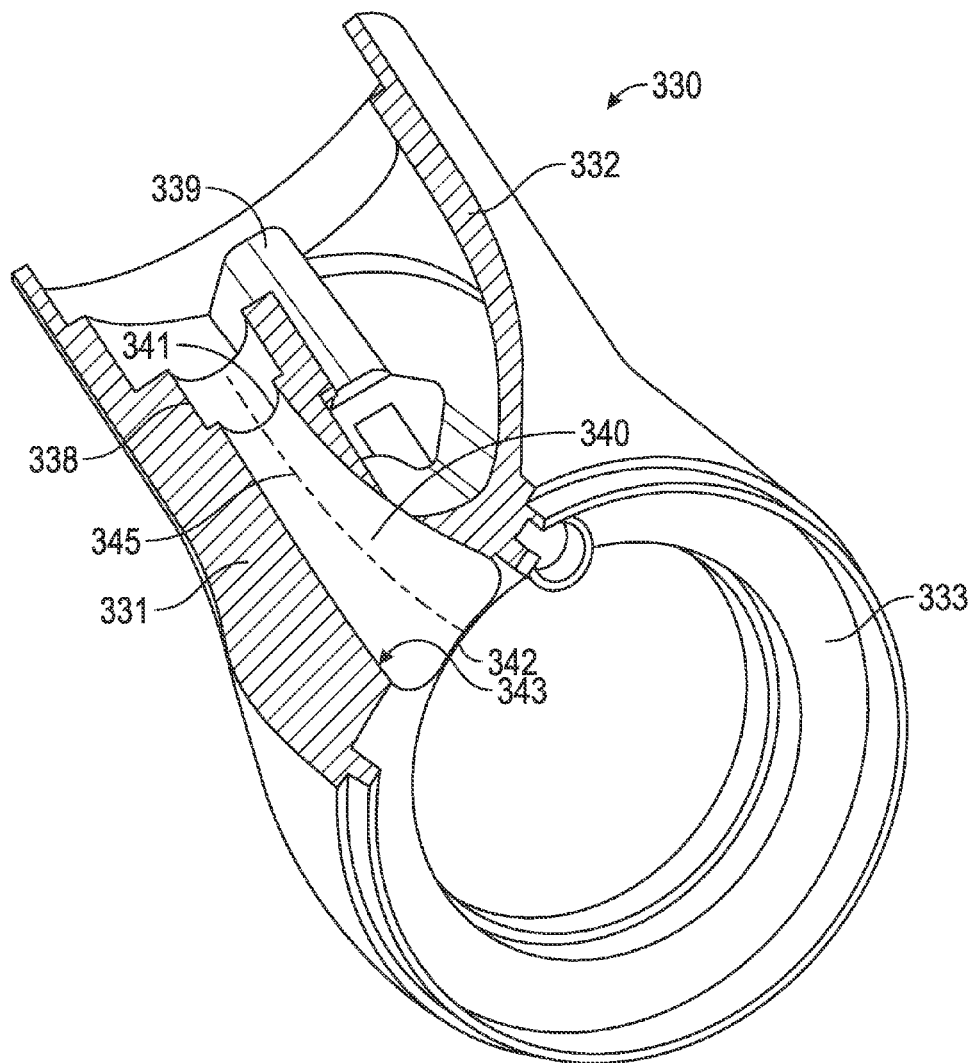


FIG. 4

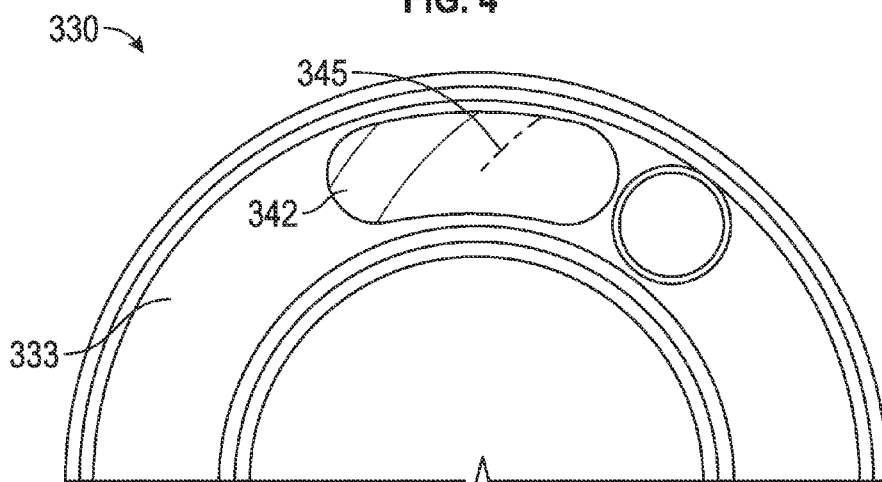


FIG. 5

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FUEL INJECTOR WITH A DIFFUSING MAIN GAS PASSAGE

TECHNICAL FIELD

The present disclosure generally pertains to gas turbine engines, and is more particularly directed toward a fuel injector with a diffusing main gas passage.

BACKGROUND

Gas turbine engines include compressor, combustor, and turbine sections. Low Wobbe gas fuels for gas turbine engines may require higher volumetric flow for the same heat input. A loss in velocity head of a Low Wobbe gas fuel may negatively affect combustion.

U.S. Pat. No. 6,848,260 to D. North discloses a combustor for a gas turbine engine with a premix pilot fuel stage in order to reduce the emission of oxides of nitrogen from the engine. An in-service engine may be modified to add the premix pilot fuel stage by delivering premix pilot fuel to a ring manifold for tip-feeding a premix pilot fuel outlet member such as a swirler vane or fuel peg. In this manner, complex and expensive components such as the top hat, support housing and diffusion pilot burner assembly may be used without modification. Thermal stresses caused by the differential cooling of the ring manifold by the premix fuel pilot are reduced by a heat shield installed within the manifold.

The present disclosure is directed toward overcoming one or more of the problems discovered by the inventors or that is known in the art.

SUMMARY OF THE DISCLOSURE

In one embodiment, the fuel injector includes a gallery enclosure and a main body adjacent the gallery enclosure. The gallery enclosure forms a gas gallery. The gas gallery is an annular passage configured to circumferentially distribute a gas fuel. The main body includes a gas passage. The gas passage includes and inlet distal to the gas gallery and an outlet adjoining the gas gallery. The inlet includes an inlet area with a circular shape. The outlet includes an outlet area including an annular sector shape. The gas passage transitions from the inlet area to the outlet area and is configured to diffuse the gas fuel and discharge the gas fuel from the outlet and into the gas gallery.

BRIEF DESCRIPTION OF THE DRAWINGS

FIG. 1 is a schematic illustration of an exemplary gas turbine engine.

FIG. 2 is a partial cut-away view of a fuel injector for the combustor of FIG. 1.

FIG. 3 is a cut-away view of the main body of the fuel injector of FIG. 2.

FIG. 4 is a front view of the main body of FIG. 3.

FIG. 5 is a front view of the main body of FIG. 3.

DETAILED DESCRIPTION

The systems and methods disclosed herein include a fuel injector with a diffusing gas passage extending between the main gas tube and the gas gallery. In embodiments, the gas passage includes an inlet with a circular cross-section and an outlet with annular sector cross-section. The gas passage may include an elliptical path and a turning angle greater

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than 0 degrees and up to 90 degrees. The diffusing gas passage with the elliptical path may prevent or reduce a loss in gas velocity head of gas discharged into the gas gallery.

FIG. 1 is a schematic illustration of an exemplary gas turbine engine 100. Some of the surfaces have been left out or exaggerated (here and in other figures) for clarity and ease of explanation. Also, the disclosure may reference a forward and an aft direction. Generally, all references to “forward” and “aft” are associated with the flow direction of primary air (i.e., air used in the combustion process), unless specified otherwise. For example, forward is “upstream” relative to primary air flow, and aft is “downstream” relative to primary air flow.

In addition, the disclosure may generally reference a center axis 95 of rotation of the gas turbine engine, which may be generally defined by the longitudinal axis of its shaft 120 (supported by a plurality of bearing assemblies 150). The center axis 95 may be common to or shared with various other engine concentric components. All references to radial, axial, and circumferential directions and measures refer to center axis 95, unless specified otherwise, and terms such as “inner” and “outer” generally indicate a lesser or greater radial distance from center axis 95, wherein a radial 96 may be in any direction perpendicular and radiating outward from center axis 95.

A gas turbine engine 100 includes an air inlet 110, a shaft 120, a compressor 200, a combustor 300, a turbine 400, an exhaust 500, and a power output coupling 600. The gas turbine engine 100 may have a single shaft or a dual shaft configuration.

The compressor 200 includes a compressor rotor assembly 210, compressor stationary vanes (stators) 250, and inlet guide vanes 255. The compressor rotor assembly 210 mechanically couples to shaft 120. As illustrated, the compressor rotor assembly 210 is an axial flow rotor assembly. The compressor rotor assembly 210 includes one or more compressor disk assemblies 220. Each compressor disk assembly 220 includes a compressor rotor disk that is circumferentially populated with compressor rotor blades. Stators 250 axially follow each of the compressor disk assemblies 220. Each compressor disk assembly 220 paired with the adjacent stators 250 that follow the compressor disk assembly 220 is considered a compressor stage. Compressor 200 includes multiple compressor stages. Inlet guide vanes 255 axially precede the compressor stages.

The combustor 300 includes one or more combustion chambers 302, one or more fuel injectors 310, and a combustor case 301 located radially outward from the combustion chamber 302. Each fuel injector 310 includes an injector head 320 adjacent the combustion chamber 302, a flange 312 adjacent the combustor case 301, and a stem 311 extending between flange 312 and injector head 320.

The turbine 400 includes a turbine rotor assembly 410 and turbine nozzles 450. The turbine rotor assembly 410 mechanically couples to the shaft 120. As illustrated, the turbine rotor assembly 410 is an axial flow rotor assembly. The turbine rotor assembly 410 includes one or more turbine disk assemblies 420. Each turbine disk assembly 420 includes a turbine disk that is circumferentially populated with single crystal turbine blades 430. Turbine nozzles 450 axially precede each of the turbine disk assemblies 420. Each turbine disk assembly 420 paired with the adjacent turbine nozzles 450 that precede the turbine disk assembly 420 is considered a turbine stage. Turbine 400 includes multiple turbine stages.

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The exhaust **500** includes an exhaust diffuser **510** and an exhaust collector **520**. The power output coupling **600** may be located at an end of shaft **120**.

FIG. 2 is a partial cut-away view of a fuel injector **310** for the combustor **300** of FIG. 1. In the embodiment illustrated, fuel injector **310** is a dual fuel injector. In other embodiments, fuel injector **310** is a gas fuel injector. Referring to FIG. 2, flange **312** may be a cylindrical disk, a cuboid or other geometric shape and may be configured to affix fuel injector **310** to combustor case **301**. Stem **311** may be a hollow cylinder shape. Stem **311** may include multiple pieces. In the embodiment illustrated, a flange stem portion **313** is an integral part of flange **312** and extends perpendicular to the cylindrical disk shape.

Fuel injector **310** includes multiple fuel/supply tubes extending between flange **312** and injector head **320**. Fuel injector **310** may include gas main tube **316**, liquid main tube **315**, gas pilot tube **318**, and other supply tubes such as tube **319** and a liquid pilot tube. Each fuel/supply tube may connect to a fitting connected to flange **312**, such as gas main fitting **306**, liquid main fitting **305**, gas pilot fitting **308**, liquid pilot fitting **307**, and supply fitting **309**. Each fitting may be connected to a fuel source, a source of compressed air, etc.

Gas main tube **316** forms a main gas passage **322** and may include a gas main tube axis **314**. Gas main tube **316** may connect to injector head **320** at an angle **325** from zero degrees to ninety degrees, angle **325** being the angle between gas main tube axis **314** and an injector head axis **321** of injector head **320**. In some embodiments, angle **325** is from thirty-five degrees to forty-five degrees. In the embodiment illustrated, the angle **325** is forty degrees. The injector head axis **321** may be parallel to center axis **95**. The other fuel/supply tubes, such as liquid main tube **315**, gas pilot tube **318**, and liquid pilot tube **317** may also connect to injector head **320** at angle **325**.

FIG. 3 is a detailed view of FIG. 2. Referring to FIGS. 2 and 3, injector head **320** is configured to include a gas gallery **355** and a gas passage **340**. Gas gallery **355** may be ring shaped passage, such as an annular passage. Gas passage **340** connects/fluidly couples main gas passage **322** to gas gallery **355**. Gas passage **340** includes an inlet **341**, an outlet **342**, and a mean camber line **345**. The cross-sectional area of gas passage **340** increases from inlet **341** to outlet **342** along the length of the mean camber line **345**.

Gas passage **340** may include a turning angle **346**. Turning angle **346** is the angle that the flow turns from inlet **341** to outlet **342** measured at the mean camber line **345**. The turning angle **346** may also be defined as the angle between the normal of the inlet cross-sectional area and the normal of the outlet cross-sectional area. Turning angle **346** may be the same angle as angle **325**. In one embodiment, turning angle **346** is greater than zero degrees and up to ninety degrees. In another embodiment, turning angle **346** is greater than zero degrees and up to forty degrees. In yet another embodiment, turning angle **346** is forty degrees.

Gas passage **340** may be configured to redirect gas fuel traveling in a direction of the gas main tube axis **314** to a direction parallel to the injector head axis **321**. Mean camber line **345** may be angled parallel to gas main tube axis **314** at the inlet **341** and may be angled parallel to injector head axis **321** at the outlet **342**.

Injector head **320** may include a main body **330**, an inlet shroud **370**, a center body **350**, a first gallery shroud **353**, and a second gallery shroud **354**. Portions of main body **330**, inlet shroud **370** center body **350**, first gallery shroud **353**,

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and second gallery shroud **354** may form a gallery enclosure **380**. The gallery enclosure **380** may define the annular shape of gas gallery **355**.

Main body **330** may include a body portion **331**, a body stem portion **332**, a gallery portion **333**, a strut **335**, and a funnel **334**. Body portion **331** may adjoin both body stem portion **332** and gallery portion **333**. In the embodiment illustrated, body portion **331** is configured to include gas passage **340**. Body portion **331** may include a gas main connection **338** and a liquid main connection **339** (shown in FIG. 3). Gas main connection **338** may be located within the body stem portion **332** and may be a protrusion formed with a cylindrical hole adjoining inlet **341** and may be sized to receive an end of gas main tube **316**. The cylindrical hole may include a diameter larger than that of inlet **341**. Liquid main connection **339** may be adjacent gas main connection **338**. Liquid main connection **339** may include a counterbore sized to receive an end of liquid main tube **315**.

Body stem portion **332** may extend from body portion **331** at angle **325** and may include a hollow cylinder shape. Body stem portion **332** may be metalurgically bonded to stem **311**. The diameters and thickness of body stem portion **332** may be the same or similar to the diameters and thickness of stem **311**.

Gallery portion **333** includes a ring like annular shape, a solid of revolution such as a toroid about an axis. The axis may be coaxial to injector head axis **321**. Gallery portion **333** may form a second or aft end of the main body **330**. Gallery portion **333** may extend circumferentially from body portion **331** and may include outlet **342**.

Gallery portion **333** may include a first axial boundary **381** and a first outer circumferential boundary **383**. The first axial boundary **381** may be an annular surface facing in the axial direction of gallery portion **333** and injector head axis **321**. First axial boundary **381** may be an axial surface of gas gallery **355**. Outlet **342** may be located at first axial boundary **381**. The first outer circumferential boundary **383** may be a cylindrical surface and may form a portion of the outer circumferential boundary of gas gallery **355**. The first outer circumferential boundary **383** may extend in the axial direction of gallery portion **333** and injector head axis **321**.

Strut **335** may extend from body portion **331** at angle **325** towards injector head axis **321**. Funnel **334** may be connected to strut **335** distal to body portion **331**. Funnel **334** may include a funnel shape. The funnel shape may revolve about or be axially aligned with injector head axis **321**. Funnel **334** may redirect pilot liquid and gas fuel from the gas pilot tube **318** and the liquid pilot tube **317** into a pilot shroud **368**.

Inlet shroud **370** may be located radially outward from pilot shroud **368** and radially inward from gallery portion **333**. Inlet shroud **370** may include a hollow cylinder shape. Inlet shroud **370** may include an inner gallery portion **372** that adjoins a radially inner portion of gallery portion **333** and extends axially from gallery portion **333** forming a portion of the radially inner boundary of gas gallery **355**. Inner gallery portion **372** may diverge at the end adjacent gallery portion **333**. Inner gallery portion **372** may include a first inner circumferential boundary **386**. The first inner circumferential boundary **386** may be a circumferential surface on the radially outer portion of the inner gallery portion **372** that is a radially inner surface of the gas gallery **355**. Inlet shroud **370** may also include an air inlet **371** distal to the gallery portion **333**.

Center body **350** may include an outer wall **348**, an inner wall **349**, and swirler vanes **361**. Outer wall **348** may adjoin inlet shroud **370** at the end of inner gallery portion **372** and

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may extend axially from inlet shroud 370. Outer wall 348 may include a hollow cylinder shape. The end portion of Outer wall 348 adjoining inlet shroud 370 may form the remainder of the radially inner boundary of gas gallery 355 and may include a second inner circumferential boundary 387 axially adjacent first inner circumferential boundary 386.

Inner wall 349 is located radially inward from outer wall 348. Inner wall 349 may also include a hollow cylinder shape. Inner wall 349 and outer wall 348 may form a portion of premix duct 369. Premix duct 369 may be an annular passage where fuel and air is mixed prior to combustion.

Swirler vanes 361 may be located proximal an end of outer wall 348 and an end of inner wall 349. Swirler vanes 361 extend radially between outer wall 348 and inner wall 349. Each swirler vane 361 may include an airfoil shape with a vane passage 363 extending radially within and one or more injection holes extending from a leading edge of the airfoil to the vane passage 363. Each vane passage 363 may extend through outer wall 348 and may be in flow communication with gas gallery 355.

First gallery shroud 353 may be a ring like shape, such as a toroid or annulus and may be axially spaced apart from gallery portion 333. First gallery shroud 353 may be located radially outward from outer wall 348 and may radially adjoin outer wall 348. The cross-sectional shape of first gallery shroud 353 may include a vertical wall extending radially from center body 350 with a radially outer leg extending towards the gallery portion 333 and a radially inner leg extending away from the gallery portion 333 along outer wall 348. First gallery shroud 353 may form a portion of the radially outer boundary of gas gallery 355 and the axially boundary of gas gallery 355 opposite gallery portion 333. The vertical wall of first gallery shroud 353 may include a second axial boundary 382 offset from first axial boundary 381. Second axial boundary 382 may be an annular surface facing in the axial direction towards first axial boundary 381. The outer leg may include a second outer circumferential boundary 384. Second outer circumferential boundary 384 may be a circumferential surface extending axially towards gallery portion 333.

Second gallery shroud 354 may radially adjoin gallery portion 333 and first gallery shroud 353 and may include a hollow cylinder shape extending across an axial space between gallery portion 333 and first gallery shroud 353. Second gallery shroud 354 may form the remainder of the outer boundary of gas gallery 355. Second gallery shroud 354 may include the third outer circumferential boundary 385. Third outer circumferential boundary 385 may be a circumferential surface extending axially between first outer circumferential boundary 383 and second outer circumferential boundary 384. Gas gallery enclosure 380 may be formed by first axial boundary 381, second axial boundary 382, first outer circumferential boundary 383, second outer circumferential boundary 384, third outer circumferential boundary 385, first inner circumferential boundary 386, and second inner circumferential boundary 387, thus defining gas gallery 355.

Injector head 320 may also include premix tube 351, barrel 352, inner premix tube 360, and swirler vanes 361. Premix tube 351 may include a hollow cylinder shape, may adjoin the end of center body 350 distal to inlet shroud 370, and may extend axially from center body 350. Barrel 352 may adjoin premix tube 351 distal to center body 350. Barrel 352 may include a barrel body 358 and a barrel flange 359. Barrel body 358 may be a hollow cylinder shape extending axially from premix tube 351. Barrel flange 359 may be a

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hollow cylinder shape located at the end of barrel body 358 distal to premix tube 351 and extending radially outward from barrel body 358.

Inner premix tube 360 extends within center body 350, premix tube 351, and barrel 352. Inner premix tube 360 may include an outer cylindrical surface. Inner premix tube 360 may form a portion of premix duct 369 with premix tube 351, and barrel 352, aft of center body 350. Inner premix tube 360 may be adjacent inlet shroud 370 and may extend axially from inlet shroud 370. Premix tube 351, barrel 352, and inner premix tube 360 may each axially align with injector head axis 321.

FIG. 4 is a cut-away view of the main body 330 of the fuel injector 310 of FIG. 2. The mean camber line 345 extending from inlet 341 to outlet 342 may follow an elliptical path from inlet 341 to outlet 342. The elliptical path may be configured to redirect the gas from the direction of the main gas passage 322 to the axial direction, a direction parallel to injector head axis 321 at turning angle 346. In some embodiments, the elliptical path may also twist/turn the mean camber line 345 in the circumferential direction relative to injector head axis 321. In one embodiment, the length of mean camber line 345 is from 7.24 cm (2.85 in.) to 7.62 cm (3.0 in.). In another embodiment, the length of mean camber line 345 is 7.44 cm (2.93 in.).

In some embodiments, the inlet cross-sectional area is from 1.21 cm² (0.188 in.²) to 1.32 cm² (0.204 in.²). In other embodiments, the inlet cross-sectional area is 1.26 cm² (0.196 in.²). In the embodiment illustrated, the cross-sectional area of inlet 341 is a circle. In some embodiments, the ratio of the length of mean camber line 345 over the radius of inlet 341 is from 11.2 to 12.2. In other embodiments, the ratio of the length of mean camber line 345 over the radius of inlet 341 is 11.7.

FIG. 5 is a front view of the main body 330 of FIG. 3. In some embodiments, outlet cross-sectional area is from 3.37 cm² (0.523 in.²) to 3.66 cm² (0.567 in.²). In other embodiments, outlet cross-sectional area is 3.52 cm² (0.545 in.²). The outlet cross-sectional area may be an annular sector. The ends of the annular sector may be rounded. In the embodiment illustrated, the outlet cross-sectional area is an annular sector with rounded, capped ends. In some embodiments, the ratio of the outlet cross-sectional area over the inlet cross-sectional area is from 1 to 4.5. In other embodiments, the ratio of the outlet cross-sectional area over the inlet cross-sectional area is from 2.5 to 3. In yet other embodiments, the ratio of the outlet cross-sectional area over the inlet cross-sectional area is 2.78.

Referring to FIGS. 4 and 5, gas passage 340 includes a surface 343 which defines the shape of gas passage 340. Surface 343 is a smooth surface that transitions from the inlet cross-sectional area of inlet 341 to the outlet cross-sectional area of outlet 342 along mean camber line 345. Surface 343 also generally diverges from the mean camber line 345 from inlet 341 to outlet 342.

Gas passage 340 is a diffuser and is configured to diffuse the gas fuel from inlet 341 to outlet 342 and discharge the gas fuel into the gas gallery 355. The shape of the gas passage 340 may also be defined by the effective total divergence angle. The effective total divergence angle for a curved diffuser may be defined as:

$$2\theta_{\text{eff}} = 2\tan^{-1}\left((A_r - 1)\frac{R}{N}\right)$$

Where $2\theta_{eff}$ is the effective total divergence angle, A_r is the area ratio of the cross-sectional area of outlet **342** over the cross-sectional area of inlet **341**, R is the radius of inlet **341**, and N is the length of the mean camber line **345**. In one embodiment, the effective total divergence angle is between 0 degrees and 10 degrees. In another embodiment, the effective total divergence angle is from 6.0 degrees to 6.5 degrees. In yet another embodiment, the effective total divergence angle is 6.3 degrees.

One or more of the above components (or their subcomponents) may be made from stainless steel and/or durable, high temperature materials known as “superalloys”. A superalloy, or high-performance alloy, is an alloy that exhibits excellent mechanical strength and creep resistance at high temperatures, good surface stability, and corrosion and oxidation resistance. Superalloys may include materials such as HASTELLOY, alloy x, INCONEL, WASPALOY, RENE alloys, HAYNES alloys, alloy 188, alloy 230, INCOLOY, MP98T, TMS alloys, and CMSX single crystal alloys.

INDUSTRIAL APPLICABILITY

Gas turbine engines may be suited for any number of industrial applications such as various aspects of the oil and gas industry (including transmission, gathering, storage, withdrawal, and lifting of oil and natural gas), the power generation industry, cogeneration, aerospace, and other transportation industries.

Referring to FIG. 1, a gas (typically air **10**) enters the air inlet **110** as a “working fluid”, and is compressed by the compressor **200**. In the compressor **200**, the working fluid is compressed in an annular flow path **115** by the series of compressor disk assemblies **220**. In particular, the air **10** is compressed in numbered “stages”, the stages being associated with each compressor disk assembly **220**. For example, “4th stage air” may be associated with the 4th compressor disk assembly **220** in the downstream or “aft” direction, going from the air inlet **110** towards the exhaust **500**). Likewise, each turbine disk assembly **420** may be associated with a numbered stage.

Once compressed air **10** leaves the compressor **200**, it enters the combustor **300**, where it is diffused and fuel is added. Gas or liquid fuel may be used. Air **10** and fuel are injected into the combustion chamber **302** via fuel injector **310** and combusted. Energy is extracted from the combustion reaction via the turbine **400** by each stage of the series of turbine disk assemblies **420**. Exhaust gas **90** may then be diffused in exhaust diffuser **510**, collected and redirected. Exhaust gas **90** exits the system via an exhaust collector **520** and may be further processed (e.g., to reduce harmful emissions, and/or to recover heat from the exhaust gas **90**).

Referring to FIGS. 2-5, when gas fuel is used, a gas fuel passage may direct the gas fuel from a supply line, such as gas main tube **316**, and into an annular manifold, such as gas gallery **355** to distribute the gas fuel to the swirler vanes **361** and mixed with the compressed air. The gas fuel discharging into the annular manifold from the gas fuel passage may result in a significant loss of gas velocity head. When a low Wobbe gas fuel is used, which may require a higher volumetric flow rate for the same heat input, the discharge may result in almost a total loss of the gas velocity head.

Gas passage **340** may be used to direct the gas fuel from gas main tube **316** to gas gallery **355**. Gas passage **340** may diffuse the gas fuel along an elliptical path, which may minimize the loss of gas velocity head as the gas fuel is discharged into the gas gallery **355**. Gas passage **340** may also be slightly twisted to avoid a liquid fuel tube. Gas

passage **340** may twist from inlet **341** to outlet **342** in a circumferential direction relative to injector head axis **321**. The area of inlet **341**, the area of outlet **342**, and the length of mean camber line **345** may be configured to reduce the losses of gas velocity head in gas passage **340** while preventing the gas fuel from stalling in the gas passage **340**.

The preceding detailed description is merely exemplary in nature and is not intended to limit the invention or the application and uses of the invention. The described embodiments are not limited to use in conjunction with a particular type of gas turbine engine. Hence, although the present disclosure, for convenience of explanation, depicts and describes a particular fuel injector, it will be appreciated that the fuel injector in accordance with this disclosure can be implemented in various other configurations, can be used with various other types of gas turbine engines, and can be used in other types of machines. Furthermore, there is no intention to be bound by any theory presented in the preceding background or detailed description. It is also understood that the illustrations may include exaggerated dimensions to better illustrate the referenced items shown, and are not consider limiting unless expressly stated as such.

What is claimed is:

1. An injector head of a fuel injector for a combustor of a gas turbine engine, the injector head comprising:
 - a gallery enclosure forming a gas gallery, the gas gallery being an annular passage configured to circumferentially distribute a gas fuel; and
 - a main body adjacent the gallery enclosure, the main body including
 - a gas passage with
 - an inlet distal to the gas gallery, the inlet including an inlet cross-sectional area with a circular shape, and
 - an outlet adjoining the gas gallery and in fluid communication with the inlet, the outlet including an outlet cross-sectional area with an annular sector shape,
 - wherein the gas passage cross-section transitions from the inlet cross-sectional area to the outlet cross-sectional area and is configured to diffuse the gas fuel and discharge the gas fuel into the gas gallery.
2. The injector head of claim 1, wherein the gas passage includes a mean camber line with an elliptical curve.
3. The injector head of claim 2, wherein the gas passage includes an effective total divergence angle between 0 degrees and 10 degrees.
4. The injector head of claim 3, wherein a ratio of the outlet cross-sectional area over the inlet cross-sectional area is from 1 to 4.5.
5. The injector head of claim 4, wherein a second ratio of a length of the mean camber line over a radius of the inlet is from 11.2 to 12.2.
6. The injector head of claim 1, wherein the outlet cross-sectional area includes a circular cap at each end of the annular sector shape.
7. The injector head of claim 1, wherein the outlet cross-sectional area is from 3.37 cm² to 3.66 cm².
8. A main body of an injector head of a fuel injector for a combustor of a gas turbine engine, the main body comprising:
 - a body stem portion including a hollow cylinder shape;
 - a body portion adjoining the body stem portion, the body portion including a gas main connection located within the hollow cylinder shape of the body stem portion;

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a gas passage including
 an inlet adjoining the gas main connection, the inlet including a circular cross-section,
 an outlet in fluid communication with the inlet, the outlet including a cross-section with an annular sector shape with circular capped ends, and
 a mean camber line extending from the inlet to the outlet with an elliptical curve,
 wherein the gas passage diverges from the mean camber line while extending from the inlet to the outlet;
 and
 a gallery portion with an annular shape adjoining the body portion distal to the body stem portion, the gallery portion including
 a first axial boundary facing in an axial direction of gallery portion, the first axial boundary being an annular surface and including the outlet of the gas passage.

9. The main body of claim 8, wherein the inlet includes a ratio of a length of the mean camber line over a radius of the inlet is from 11.2 to 12.2.

10. The main body of claim 9, wherein a ratio of the outlet cross-sectional area over the inlet cross-sectional area is from 2.5 to 3.

11. The main body of claim 9, wherein the gas passage includes an effective total divergence angle from 6 degrees to 6.5 degrees, smoothly transitioning from the circular cross-section of the inlet to the cross-section with the annular sector shape having circular capped ends of the outlet.

12. The main body of claim 8, wherein the gas passage includes a turning angle greater than 0 and up to ninety degrees.

13. The main body of claim 8, wherein the cross-section of the outlet is from 3.37 cm² to 3.66 cm².

14. A fuel injector for a combustor of a gas turbine engine, the fuel injector comprising:

- a flange;
- a gas main fitting connected to the flange and configured to couple to a gas fuel source;
- a gas main tube coupled to the gas main fitting and extending along a first axis;
- an injector head spaced apart from the flange and extending along a second axis angled from 35 degrees to 45 degrees relative to the first axis, the injector head including
- a main body including
 - a body portion including a gas main connection coupled to the gas main tube distal to the fitting, and

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- a gallery portion coaxial to the second axis and extending from the body portion in a circumferential direction, forming a ring shape,
- an inlet shroud including an inner gallery portion adjoining the gallery portion and located radially inward from the gallery portion,
- a center body including
 - an outer wall extending from the inner gallery portion, the outer wall including a first hollow cylinder shape,
 - an inner wall located radially inward from the outer wall, the inner wall including a second hollow cylinder shape, and
 - swirler vanes extending radially between the outer wall and the inner wall, each swirler vane including a vane passage extending radially,
- a gas gallery formed by a gallery enclosure including a portion of the gallery portion, a portion of the inner gallery portion, and a portion of the outer wall, the gas gallery being an annular passage in flow communication with each vane passage, and
- a gas passage including
 - an inlet adjoining the gas main connection and in flow communication with the gas main tube, the inlet including an inlet cross-sectional area with a circular shape,
 - an outlet adjoining and in flow communication with the gas gallery, the outlet including an outlet cross-sectional area including an annular sector shape, and
 - a mean camber line extending from the inlet to the outlet, wherein the gas passage diverges from the mean camber line and transitions smoothly from the inlet to the outlet.

15. The fuel injector of claim 14, wherein the mean camber line is angled parallel to the first axis at the inlet and parallel to the second axis at the outlet.

16. The fuel injector of claim 14, wherein the gas passage includes an effective total divergence angle from 6 degrees to 6.5 degrees.

17. The fuel injector of claim 14, wherein the mean camber line twists from the inlet to the outlet in a circumferential direction relative to the second axis.

18. The fuel injector of claim 14, wherein the mean camber line is an elliptical curve extending from the inlet to the outlet.

19. The fuel injector of claim 14, wherein a ratio of the outlet cross-sectional area over the inlet cross-sectional area is from 2.5 to 3.

20. A gas turbine engine including the fuel injector of claim 14.

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